

**PCT**WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau

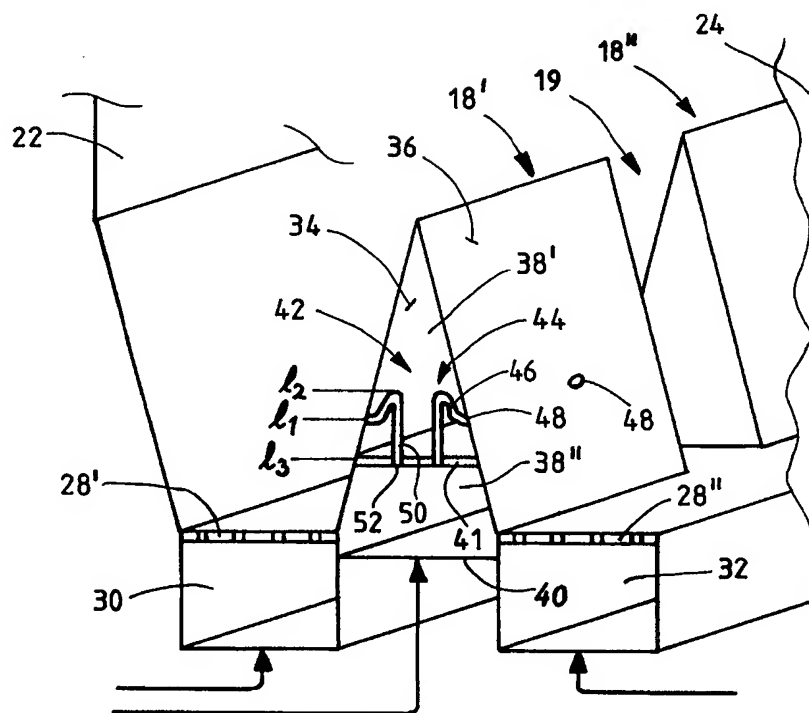
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶ : F23C 11/02 // F23L 9/00, B01J 8/24		A1	(11) International Publication Number: WO 99/02920
			(43) International Publication Date: 21 January 1999 (21.01.99)
(21) International Application Number: PCT/FI98/00560 (22) International Filing Date: 26 June 1998 (26.06.98) (30) Priority Data: 08/888,790 7 July 1997 (07.07.97) US (71) Applicant: FOSTER WHEELER ENERGIA OY [FI/FI]; Sentnerikuja 2, FIN-00440 Helsinki (FI). (72) Inventors: WIETZKE, Donald, L.; 7832 Quebrada Circle, Carlsbad, CA 92009 (US). RASKIN, Neil, R.; 7322 Muslo Lane, Carlsbad, CA 92009 (US). DARLING, Scott; 17 Pine Place, Annandale, NJ 08801 (US). (74) Agent: TURUN PATENTTITOIMISTO OY; P.O. Box 99, FIN-20521 Turku (FI).		(81) Designated States: AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GE, GH, GM, GW, HU, ID, IL, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG). Published <i>With international search report.</i> <i>With amended claims.</i>	

(54) Title: FLUIDIZED BED REACTOR

(57) Abstract

A fluidized bed reactor including in its lower part a furnace section having a bed of fluidized solid particles, the furnace section being delimited by side walls such as external side walls (22, 24) and/or partition walls (34, 36) and a bottom grid (28', 28''), and a supplying device for introducing gas, e.g. secondary air, into the furnace section at a level above the bottom grid, the supplying device including a gas source chamber (38'), an opening (48) in at least one of the side walls at a level above the bottom grid, and a conduit (42, 44) having a first end connected to the opening and a second end (52) connected to the gas source chamber. The conduit includes a solid flow seal preventing solid particles from flowing backwards from the furnace section into the conduit in a manner preventing or noticeably decreasing introduction of gas from the gas source chamber to the furnace section.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav	TM	Turkmenistan
BF	Burkina Faso	GR	Greece		Republic of Macedonia	TR	Turkey
BG	Bulgaria	HU	Hungary	ML	Mali	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MN	Mongolia	UA	Ukraine
BR	Brazil	IL	Israel	MR	Mauritania	UG	Uganda
BY	Belarus	IS	Iceland	MW	Malawi	US	United States of America
CA	Canada	IT	Italy	MX	Mexico	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NE	Niger	VN	Viet Nam
CG	Congo	KE	Kenya	NL	Netherlands	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NO	Norway	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's	NZ	New Zealand		
CM	Cameroon		Republic of Korea	PL	Poland		
CN	China	KR	Republic of Korea	PT	Portugal		
CU	Cuba	KZ	Kazakistan	RO	Romania		
CZ	Czech Republic	LC	Saint Lucia	RU	Russian Federation		
DE	Germany	LI	Liechtenstein	SD	Sudan		
DK	Denmark	LK	Sri Lanka	SE	Sweden		
EE	Estonia	LR	Liberia	SG	Singapore		

FLUIDIZED BED REACTOR

The present invention refers to a fluidized bed reactor
5 having in its lower part a furnace section, delimited by
side walls and a bottom grid, and supplying means, for
introducing a gas, such as partial combustion air, into a
bed of fluidized particles in the furnace section. Such
supplying means include a gas source chamber, such as a
10 windbox and at least one nozzle or conduit connected to one
opening in a side wall, for introducing gas from said gas
source chamber to the furnace section.

This invention is particularly applicable to large
15 circulating fluidized bed (CFB) boilers having a thermal
effect of, e.g., 200-400 MWe, or more, in which boilers the
lower section of the boiler furnace and the bottom grid may
be divided in two or more furnace sections, e.g. by a dual
wall partition structure. The dual wall partition structure
20 may be a complete partition wall reaching in the furnace
from one wall to the opposite wall or a partial wall, i.e.
the dual wall construction may consist of a continuous or
a discontinuous wall between two opposite furnace walls. In
these large boilers partial air may be distributed through
25 supplying means connected to the external side walls and/or
to supplying means connected to the partition wall
structure. The partition wall structure, which typically is
of a dual wall construction may be made a refractory wall
or a cooled wall connected to the cooling water circulation
30 of the boiler.

BACKGROUND OF THE INVENTION

Optimized emission control and maximum fuel burn-up are
35 decisive qualifications for a successful furnace design.
Thus, they must especially be taken into consideration in
circulating fluidized bed scale-up. A simple proportional
scaling up of designs used in smaller systems may easily
lead to problems in attempting to provide for a good mixing
40 of fuel, combustion air and fluidized bed solids.
Additionally, such designs may suffer from not being

capable of providing a uniform furnace temperature within the optimum range and a sufficient heat transfer area. All these problems, which may cause enhanced emissions and less than optimal fuel burn-up, have led to a desire to find
5 alternative solutions. Such solutions have e.g. included designs with multiple furnaces with a common back pass, providing heat transfer panels and/or partial or full division walls within the furnace, or dividing the lower part of the furnace and the bottom grid with e.g. a dual
10 wall structure.

Different solutions for sectioning the bottom area of a fluidized bed boiler furnace are known in the prior art. US patent 4,864,944 discloses a division of a fluidized bed
15 reactor into compartments by partition walls having openings for secondary gas to be distributed in a desired manner into the reactor. The partition walls have ducts which are connected to air supply sources and lead to discharge openings at different heights in the partition
20 walls. Correspondingly, US patent 4,817,563 discloses a fluidized bed system provided with one or more displacement bodies, which may be provided with lines and inlet openings for introducing secondary gas to segmented sections in the lower reactor.

25 US patent 5,370,084 discloses different configurations for effective mixing of fuel in a partitioned circulating fluidized bed boiler, including ducts which feed air into the boiler on the interior walls. US patent 5,215,042
30 discloses a CFB reactor divided into compartments by at least one vertical, substantially gas tight partition in the upper part of the combustion chamber. The partition wall comprises cooling tubes and is provided with at least one line with a distributing manifold to feed combustion
35 air into the compartments.

US patent 4,545,959 discloses a chamber for the treatment

of particulate matter in a fluidized bed, comprising a duct with triangular cross section on the bottom of the chamber, and an arrangement of holes or slots in each of the upwardly sloping side walls of the duct for directing an ancillary gas from the duct into the chamber.

The above mentioned publications suggest introduction of gas into a reactor chamber, e.g. furnace chamber, through a partition wall within the chamber. A problem arises, however, as the ducting from the air or gas source chamber to the air or gas injection point may be rather long and cause a high pressure drop. A problem arises also in these conventional supply duct constructions due to solids back sifting, i.e. the problems with solid particles from the furnace tending to flow into the gas supply ducts and increase the pressure drop over the gas supply ducts. The increase in pressure drop may be very difficult to attend to or to take into consideration when controlling the gas supply.

20

Conventional bottom grid nozzle constructions, e.g. those equipped with bubble caps normally reaching upward from the bottom grid, would be exposed to heavy erosion if installed on a vertical partition wall within a fluidized bed, due to very high erosive forces caused by the downward flowing solid particle layers in the vicinity of the wall. In fluidized bed reactor furnaces solid particles tend to flow upward in the middle of each furnace section and downward along its vertical side walls. Such downward flowing particles come in the lower part of the furnace sections, when the cross sectional area of the furnace sections abruptly decreases, into intense turbulent motion which may locally lead to very strong erosive forces, e.g. also in the regions of secondary gas inlets. In the prior art no special solution for preventing backsifting into gas nozzles or conduits arranged on partition walls has been disclosed.

It is therefore an object of the present invention to provide a fluidized bed reactor with a furnace construction with an improved gas supply configuration.

5 It is particularly an object of the present invention to provide an improved gas supply configuration suitable for large scale circulating fluidized bed (CFB) boilers.

It is then more specifically an object of the present
10 invention to provide an improved secondary gas supply configuration arranged in a partition wall within the lower part of a boiler furnace.

It is more specifically an object of the present invention
15 to provide a fluidized bed reactor with improved gas supply means, with minimized backsifting of solid particles into gas supply conduits therein.

It is thereby also an object of the present invention to
20 provide a fluidized bed reactor with improved gas supply means with decreased pressure losses in the gas supply means.

SUMMARY OF THE INVENTION

25

These and other objects of the present invention are achieved in a fluidized bed reactor by arranging in the lower part of a furnace section therein, which furnace section is delimited by side walls and a bottom grid, a
30 supplying means including

- a gas source chamber, such as a windbox,
- at least one opening in at least one of said side walls at a level above the bottom grid, and
- at least one conduit, connected by its one end
35 to said at least one opening and by its other end to said gas source chamber, for introducing gas from said gas source chamber to said furnace

section,
whereby, said at least one conduit comprises a solid flow seal, preventing solid particles from flowing backward from said furnace section into said at least one conduit in a manner preventing or noticeably decreasing said introduction of gas from said gas source chamber to said furnace section.

In large scale fluidized bed reactors, divided by dual-wall partitions into separate furnace sections, at least a part of the free internal space between the partition walls may according to a preferred embodiment of the present invention constitute the gas source chamber or windbox, providing secondary or other gas to the furnace sections. The gas source chamber may on the other hand if desired according to another preferred embodiment of the present invention be formed at another location also, e.g. connected to an external side wall or to the bottom grid.

Secondary gas or other similar gas is typically introduced into furnace sections through a plurality of gas injecting openings formed in the side walls delimiting the furnace sections. The openings may be arranged in a single row at the same vertical level in each wall, or the openings may if desired be arranged in some other configuration and at several different vertical levels in the walls. A conduit, such as a standpipe or a bent pipe construction, is according to the present invention disposed between each of the openings and a gas source chamber, for introducing gas from the gas source chamber through the openings into the furnace sections.

A solid flow seal is formed in the conduits so as to prevent solid particles from flowing backward into the conduit in a manner preventing or noticeably decreasing the introduction of gas from the gas source chamber to the furnace sections. Some minor back and forth flow of solid

particles within the conduits close to the openings may be tolerable. The solid flow seals may be formed in different ways, e.g. depending on the location of the gas source chamber.

5

In a fluidized bed reactor, in which the gas source chamber is formed in the space between two partition walls forming a partition on the bottom grid, secondary gas/air nozzles or conduits in the form of openended standpipes may preferably be used. The standpipes have a first open end connected to an opening in one of the partition walls at a first vertical level l_1 , e.g. at the secondary air injection level, and a second open end opening into the gas source chamber at a second vertical level l_2 which is at a higher level than the first vertical level. This construction may be used when at least a portion of the gas source chamber reaches to a vertical level above the injection level of the gas, e.g. the injection level of secondary air.

20

The standpipe preferably has a circular cross section, but other forms are possible, such as slot like cross sections. The vertical extent of the standpipe, i.e. the difference $l_2 - l_1$, has to be big enough to generally prevent solid particles from backsifting therethrough from the furnace section to the gas source chamber.

The standpipe may be bent at its lower end, such that the lower end thereof may be fastened more easily to a vertical or only slightly inclined side wall construction. The standpipe may even have a short nearly horizontal lower portion in order to bring the standpipe out from the side wall construction. Preferably a minimum distance or clearance is provided between the side wall and the standpipe along the entire length of the standpipe, i.e. also when the side wall is inclined and approaches the standpipe at the upper end thereof. Another solution would

be to make the standpipe slightly inclined.

The standpipe is, however, preferably substantially upright, but may due to constructional reasons and as
5 discussed above have a lowermost portion, forming a $< 90^\circ$, typically about 45° , but always $\geq 30^\circ$ angle with the horizontal plane. The rest of the standpipe, i.e. the upper portion of the standpipe, is mainly upright forming a $\geq 30^\circ$ angle with the horizontal plane.

10

In a fluidized bed reactor having a gas source chamber at a substantially different location, e.g. partly or totally above or below the grid level, another conduit or nozzle construction may be used in order to bring up gas from the
15 gas source chamber to e.g. the secondary gas level. The conduit, which may be formed of a pipe or other similar element, has according to a preferred embodiment of the present invention the form of an upside down U-bend. A first end of the conduit is connected to an opening at a
20 first vertical level l_1 in one of the side walls and a second end of the conduit is connected at a third vertical level l_3 to an opening in an enclosure delimiting the gas source chamber. The conduit has between its first and second ends an upward bent portion, having its highest
25 point at a second vertical level l_2 , which is at a higher level than the first l_1 and third l_3 vertical levels. The first level, i.e. the secondary air injection level, typically is at a higher level than the third level, which may be e.g. at the bottom grid level or below or above the
30 grid level.

The vertical extent of an upright standpipe or the height of the first portion of a bent conduit, correlates to the solid flow backsifting preventing ability of the conduit.
35 The height difference Δl between the first l_1 and second l_2 vertical levels is directly related to the pressure required to move solid particles through the standpipe,

e.g.. the larger the Δl the longer the standpipe, and the less solid particles are able to backsift through the conduit.

- 5 Typically, a vertical column Δl of about 1.0 meters may be needed for providing an efficient solid flow seal against normal furnace pressure variations.

The constructions described above may be used, as discussed
10 earlier, in fluidized bed reactors having the lower part of the furnace section divided by a dual-wall partition. Such a partition may if desired reach from the bottom grid up to the roof of the furnace, dividing the entire furnace chamber in two separate sections. Such furnace dividing
15 walls preferably include at least one opening in their upper part to allow horizontal mixing of the gases and fluidized particles in the separate furnace sections.

The partition walls dividing the lower part of the furnace
20 or the divisional walls dividing the entire furnace into two parts or sections may preferably be constructed of finned tube panels, where the flow direction of the cooling medium is upwards from a header on the level of or below the furnace bottom. The cooling tubes of a partition wall
25 may extend substantially vertically up to the roof of the furnace thus forming a divisional wall within the furnace, the tubes providing additional cooling surface area within the furnace.

30 In many known fluidized bed reactor constructions the interior of dual wall partitions contain various ducts for different purposes, but the interior space formed between the partition walls has not been otherwise utilized. When using, according to the present invention, at least a part
35 of the interior of the dual wall partition as a windbox for air or gas, which is to be distributed into the furnace above the primary air grid, space is correspondingly spared

below the main furnace grid. Moreover, the required length of ducting between windbox and air/gas introduction point in the furnace is minimized, which leads to decreased pressure losses, i.e. lower cost, compared to conventional constructions. The present invention then provides, due to the decreased pressure losses, a better air/gas distribution and hence more optimal reaction conditions within the furnace. Also by locating structures preventing back sifting of solid particles into the interior of a dual wall partition, the structures are protected from the erosive forces of moving solids in the vicinity of the partition.

BRIEF DESCRIPTION OF THE DRAWINGS

The above brief description, as well as further objects, features and advantages of the present invention will be more fully appreciated by reference to the following detailed description of the presently preferred but nonetheless illustrative embodiments in accordance with the present invention when taken in conjunction with the accompanying drawings in which

FIG. 1 schematically shows a vertical cross section of a first exemplary fluidized bed reactor according to the present invention;

FIG. 2 schematically shows a vertical and partly axonometrical cross section of the lower part of the fluidized bed reactor shown in FIG. 1;

FIG. 3 schematically shows a vertical cross section of a second fluidized bed reactor according to the present invention;

FIG. 4 schematically shows a vertical cross section of the lower part of the second fluidized bed reactor shown in FIG. 3, and

FIG. 5 schematically shows an enlargement of a cross section of a standpipe connected to a side wall

according to the present invention.

DETAILED DESCRIPTION OF THE DRAWINGS

5 Referring now specifically to FIG. 1 and FIG. 2 of the drawings, the reference numeral 10 refers, in general, to the fluidized bed reactor, having a furnace 12, the lower part of which is divided in two furnace sections 14 and 16 by a partition 18, having a dual wall construction. The
10 partition 18 is in FIG. 2 shown as a discontinuous partition consisting of partial partitions 18' and 18'' separated by an intermediate free portion 19 allowing solids and gas flow from one furnace section 14, 16 to the other 16, 14. The discontinuous partition shown in FIG. 2
15 is one example of a solids and gas flow path between furnace sections 14, 16, other embodiments not shown in these example drawings include one or more conduits through the partition wall; a partial partition dual wall construction; and others. A fluidized bed of solid
20 particles 20 is maintained in the furnace 12. The furnace has external side walls 22 and 24, a roof 26 and a bottom grid 28. Fluidizing air or gas is introduced into the furnace sections 14 and 16 through grid parts 28' and 28'' from windboxes 30 and 32.

25

The partition 18, i.e. the partial partitions 18' and 18'', dividing the lower part of the furnace 12, is of a dual wall construction, i.e. formed of two inclined partition walls, i.e. a first 34 and a second 36 partition wall.
30 Thereby a partition space 38, or an internal space of the partition, is delimited by the partition walls 34 and 36 and a bottom 40 covered by the partition. The bottom 40 is in FIG. 2 shown to be disposed slightly below the grid 28 level, but could be formed at the same level as the grid
35 or even above the grid level. A free space is formed between the windboxes 30 and 32 which can be used for other purposes. The gas space 38 between the partition walls 34

and 36 is divided by a horizontal nozzle supporting partition 41 into an upper 38' and a lower 38'' gas space.

Nozzles or conduits 42 and 44 according to the invention
5 are disposed in two rows in the partition space 38' on the nozzle supporting partition or plate 41. The conduits 42 and 44 are made of tubes or pipes formed as upside down U-bends, one leg being longer than the other. The first conduits 42 are connected by their shorter legs 46, i.e.
10 the first ends of the conduits, to openings 48 in the partition wall 34 at a first vertical level l_1 . The shorter legs 46 reach within the partition space 38' upward from the openings 48 to a second vertical level l_2 , i.e. the highest point of the U-bend. The first conduits 42 are
15 further connected by their longer legs 50, i.e. the second ends of the conduits, at a third vertical level l_3 to openings 52 in the nozzle supporting partition 41, the openings opening into a windbox or gas source chamber formed in the gas space 38'' between the bottom 40 and the
20 nozzle support partition 41. Similarly the other bent conduits 44 are connected to openings, in partition wall 36 and nozzle supporting partition 41.

The height difference $\Delta l = l_2 - l_1$ between the first ends of
25 conduits 42 or 44 and the highest points of the conduits, i.e. of the U-bends, which corresponds to the vertical extension of the shorter legs 46 of the conduits, provides a solid flow seal. The pressure provided by the leg of solids against the counterflowing gas stream within the
30 conduit then prevents particles from flowing from the furnace sections 14 and 16 upward into the conduits in such a manner that a severe pressure drop affecting gas flow through the conduits would arise. The solid flow seal also prevents backsifting of solid particles through the entire
35 conduits 42, 44 from the furnace to the windbox 38''.

Thereby in the FIG. 1 and 2 embodiment openings 48,

conduits 42, 44, including first legs 46 and second legs 50, as well as, a windbox 38'' constitute e.g. a secondary gas supplying means for the fluidized bed reactor.

5 FIG. 3, 4 and 5 show another preferred embodiment of the present invention. Same reference numerals as in FIGS. 1 and 2 have been used where applicable. In this embodiment a partition 18 reaches from the bottom grid 28 to the roof 26 dividing the entire furnace into two sections 14 and 16.
10 A discontinuous partition, as indicated by reference numeral 19 in FIG. 2, or other similar solids and gas communication conduit between the furnace sections 14 and 16 may also be provided. The lowermost portion of the partition 18 comprises two partition walls 34, 36, forming
15 a pyramidal free space 39 between the partition walls. The space 39 between partition walls 34 and 36 and a bottom plate 56 is used as a windbox or gas source chamber for the gas supplying means. The gas source chamber may be divided by a horizontal partition 54, as shown in FIG. 4, into an
20 upper 39' and a lower 39'' windbox.

The bottom plate 56 is disposed at the bottom grid level 28, but could be disposed above or below said level. A free space 58 is due to this construction formed below the grid
25 level between the fluidizing air windboxes 30, 32, which space may be used for locating ancillary elements which otherwise would have to be located on the periphery of the reactor. The reactor's total footprint area may thus be used more efficiently.

30

In this embodiment the gas the injecting conduits 60, 62 are simple upright open ended standpipes located within the lower partition space 39'', the space thus forming a windbox. The standpipes are connected by their lower ends
35 64 at a vertical level l_1 to openings 48 in the partition walls 34, 36. The upper free ends 66 of the conduits reach upward within the partition space 39 to a vertical level

1₂. The difference Δl in height between levels l_1 and l_2 provides the solid flow seal preventing solid flow upward in the conduits 60, 62 and into the partition space 39''.

5 Air is supplied from the free gas space or windbox 39'' through conduits 60, 62, e.g. as secondary air into the furnace sections 14 and 16. The air flows from the windbox 39'' into the standpipes 60 and 62 at their upper open ends 66 and further downward through the standpipes, via a bend
10 63 at the lower end of the standpipes and through openings 48 into the furnace. The lower end of the standpipes is bent for better enabling a fixing of the standpipes to the openings 48 in the generally vertical walls 34, 36.

15 FIG. 5 shows more clearly an exemplary position of a standpipe 60, connected to opening 48 in partition wall 34. The lower end 64 of the standpipe is disposed almost horizontally, upwardly inclined in an angle $\geq 30^\circ$ but $< 90^\circ$ to the horizontal plane, in order for the standpipe to be
20 able to stand out from the wall. The upper or main part 66 of the standpipe is almost vertical, inclined in an angle $\beta > 45^\circ$ to the horizontal plane.

Typically all secondary air or gas conduits are arranged to
25 introduce air or gas at a certain predetermined level. There may, however, be conduits at different levels, as well. Thus conduits 60' and 62' (in FIG. 4) may be used to introduce tertiary air at a higher level than conduits 60 and 62. The tertiary air conduits 60' and 62' are as shown
30 in FIG. 4 located in the separate upper portion 39' of the free gas space 39. The horizontal partition 54 dividing the free gas space into separate lower and upper gas spaces enables separate control of e.g. secondary and tertiary air injection. Vertical partition walls may also be used (not
35 shown in the drawings) to divide the free gas space further and to enable separate control of gas injected to the separate furnace sections 14 and 16.

There may also be conduits connected to openings in the external side walls 22 and 24. Such a conduit 68 is depicted in FIG. 4. The conduit is located in a windbox 70 connected to the external side wall 22.

5

While the invention has been described in connection with what is presently considered to be the most practical and preferred embodiment, it is to be understood that the invention is not to be limited to the disclosed embodiment,
10 but on the contrary, is intended to cover various modifications and equivalent arrangements included within the spirit and scope of the appended claims.

Therefore, even if the present invention has mainly been
15 described in connection with large fluidized bed boilers having a partition dividing the furnace into two or more sections, the conduit constructions according to the present invention may, however, be applied in non-divided furnace reactors as well. Then the upright conduits are
20 connected to external walls and gas source chambers in connection therewith.

Also the present new conduit construction may, of course, be used to feed other suitable fluid, such as some
25 ancillary fluid or air and fuel mixtures, into a furnace.

What is claimed is:

1. A fluidized bed reactor comprising in its lower part
- at least one furnace section, said at least one furnace
5 section being delimited by side walls, such as external
side walls and/or complete or partial partition walls, and
a bottom grid, said at least one furnace section further
having a bed of fluidized solid particles therein, and
- supplying means, for introducing a gas, such as partial
10 combustion air, into the at least one furnace section at a
level above the bottom grid, said supplying means including
- a gas source chamber, such as a windbox,
- at least one opening in at least one of said
side walls at a level above the bottom grid, and
15 - at least one conduit having a first end
connected to said at least one opening at a first
vertical level l_1 and a second end connected to
said gas source chamber, for introducing gas from
said gas source chamber to said at least one
20 furnace section,
whereby, said at least one conduit comprises a solid flow
seal, preventing solid particles from flowing backward from
said at least one furnace section into said at least one
conduit in a manner preventing or noticeably decreasing
25 said introduction of gas from said gas source chamber to
said at least one furnace section.

2. A fluidized bed reactor according to claim 1, wherein
the solid flow seal is formed by the conduit having
30 - a highest point at a second vertical level l_2 , which
second vertical level l_2 is higher than the first vertical
level l_1 .

3. A fluidized bed reactor according to claim 1 or 2,
35 wherein the supplying means include
- a plurality of openings at the same vertical
level in at least one of the side walls, and

- one of said at least one conduits being connected to each of said openings.

4. A fluidized bed reactor according to claim 1, wherein
5 the solid flow seal is formed by the at least one conduit comprising

- a second end within a gas source chamber, such as a windbox, at a vertical level higher than the first vertical level.

10

5. A fluidized bed reactor according to claim 2, wherein said second end is at a second vertical level l_2 .

6. A fluidized bed reactor according to claim 4 or 5,
15 wherein the conduit is a mainly upright standpipe, having a bent lower portion connecting said standpipe to the opening in the side wall.

7. A fluidized bed reactor according to claim 1, wherein
20 the conduit is a standpipe having

- a lower upward inclined portion, the axis thereof forming a $\geq 30^\circ$ but $< 90^\circ$ angle with the horizontal plane, and
- an upper portion, the axis thereof forming a $> 45^\circ$ angle with the horizontal plane.

25

8. A fluidized bed reactor according to claim 2, wherein
- said second end is connected at a third vertical level l_3 to an opening in an enclosure delimiting said gas source chamber,

30 said conduit having said highest point at an upward bent portion of the conduit, between its first and second end.

9. A fluidized bed reactor according to claim 8, wherein the gas source chamber is at least partly above the bottom
35 grid and the first vertical level is above the third vertical level.

10. A fluidized bed reactor according to claim 1, wherein the solid flow seal is formed by the conduit having
- a first substantially upright conduit portion connected by its lower end to one of said at least one openings at a first vertical level in a side wall,
 - a second substantially upright conduit portion connected by its lower end to an air distributor plate connected to a gas source chamber, such as a windbox, at a third vertical level, and
 - the upper ends of said first and second conduit portions being connected to each other at a second vertical level, higher than said first level.

11. A fluidized bed reactor according to claim 10, wherein the third vertical level l_3 is lower than the first vertical level l_1 .

12. A fluidized bed reactor according to claim 1 or 2, wherein
- the fluidized bed reactor comprises two furnace sections which are separated from each other by a partition and
 - supplying means for introducing gas into the furnace sections are connected to the partition.

13. A fluidized bed reactor according to claim 1, wherein
- the fluidized bed reactor comprises two furnace sections separated by a partition, which is a double wall construction, formed of two substantially upright or inclined partition walls delimiting a partition space between them, and
 - the supplying means for introducing gas into the furnace sections are connected to the partition and include
 - openings in the partition walls and
 - conduits arranged within the partition space and connected by their first ends to said openings in the partition walls and being by their second ends in flow communication with said gas source

chamber.

14. A fluidized bed reactor according to claim 13, wherein
- a part of the partition space between the two
5 partition walls forms the gas source chamber, and
- the conduits are standpipes arranged within said
gas source chamber.

15. A fluidized bed reactor according to claim 13, wherein
10 - the partition space is delimited at its vertical
sides by the two partition walls and at its bottom
by a nozzle supporting plate separating the
partition space from the gas source chamber, and
- the conduits arranged within the partition space
15 are connected by their second ends to openings in
the nozzle supporting plate, for providing gas
from the gas source chamber to the furnace
sections.

20 16. A fluidized bed reactor according to claim 13, wherein
the partition is made of cooling surfaces.

17. A large circulating fluidized bed boiler, comprising a
combustion chamber delimited by side walls, a bottom grid
25 and a roof, the side walls being made of cooling surfaces,
such as finned tube panels or membrane walls, forming a
part of the water/steam system of the boiler,
- the combustion chamber being divided by at least one
division wall reaching mainly from the bottom grid to the
30 roof, for forming two or more separate combustion sections
in said combustion chamber, said at least one division wall
being made of cooling surfaces connected to said water/
steam system of the boiler,
- the lowermost part of the at least one division wall
35 being formed as a dual wall section, the dual wall section
being continuous or discontinuous or having solids/ gas
flow paths between the separate combustion chamber

- sections, and
- a free gas space being formed between the two walls in the dual wall section, and wherein
- 5 - secondary air conduits are provided in the gas space between the walls of the dual wall section, the inlet ends of the conduits being connected to a windbox and the outlet ends of the conduits to openings in the walls of the dual wall section, for introducing air from the windbox into the
- 10 combustion sections, and
- the secondary air conduits comprising a solid flow seal, preventing solid particles from flowing backward from said combustion section into said conduit in a manner preventing air flow through said secondary conduit.
- 15
18. A fluidized bed boiler according to claim 17, wherein
- the windbox is formed in the free gas space between the walls of the dual wall,
 - the conduits are disposed in said windbox, and
- 20 - the conduits are mainly upright standpipes connected
- by their lower ends, which are the outlet ends of the air conduits, at a first vertical level l_1 to openings in the walls of the dual wall section, and
- 25
- by their upper ends to the windbox, the upper ends being the inlet ends of the air conduits and located at a second vertical level l_2 higher than the first vertical level.
- 30 19. A fluidized bed boiler according to claim 18, wherein the height difference Δh between the first l_1 and second l_2 vertical level is about 1.0 m to provide a seal leg by the pressure difference between the windbox and the combustion section.
- 35
20. A fluidized bed boiler according to claim 17, wherein
- the free gas space is divided by a horizontal partition

- . into an upper and a lower free gas space;
 - the secondary air conduits in said lower free gas space are connected to a row of openings at a first level in the walls of the partition, and additionally
 - 5 - tertiary conduits are provided in said upper free gas space and connected to a row of openings at a second level in the partition.

21. A fluidized bed boiler according to claim 17, wherein
- 10 - the free gas space is divided by a vertical partition.

AMENDED CLAIMS

[received by the International Bureau on 4 December 1998 (4.12.98);
original claims 1,3,6,10 and 12 amended; remaining claims unchanged (6 pages)]

1. A fluidized bed reactor comprising in its lower part
- a furnace (12), delimited by side walls (22, 24), and a
5 bottom grid (28), said furnace further having a bed of
fluidized solid particles therein,
- a partition (18) extending within the furnace from the
grid upward, said partition being formed as a double wall
construction of two upright or inclined partition walls
10 (34, 36), and
- supplying means, for introducing a gas, such as partial
combustion air, into the furnace at a level above the
bottom grid, said supplying means including
- a gas source chamber (38'''), such as a windbox,
15 disposed at least partly within said partition,
- at least one opening (48) in at least one of
said partition walls (34, 36) at a level above the
bottom grid, and
- at least one conduit (42, 44) having a first end
20 (46) connected to said at least one opening at a
first vertical level l_1 and a second end (50)
connected to said gas source chamber (38'''), for
introducing gas from said gas source chamber to
said furnace,
25 whereby, said at least one conduit comprises a solid flow
seal, preventing solid particles from flowing backward from
said furnace into said at least one conduit in a manner
preventing or noticeably decreasing said introduction of
gas from said gas source chamber to said furnace.
30
2. A fluidized bed reactor according to claim 1, wherein
the solid flow seal is formed by the conduit having
- a highest point at a second vertical level l_2 , which
second vertical level l_2 is higher than the first vertical
35 level l_1 .
3. A fluidized bed reactor according to claim 1 or 2,

wherein the supplying means include

- a plurality of openings at the same vertical level in at least one of the partition walls, and
 - one of said at least one conduits being
- 5 connected to each of said openings.

4. A fluidized bed reactor according to claim 1, wherein the solid flow seal is formed by the at least one conduit (60, 60', 62, 62') comprising

- 10 - a second end within a gas source chamber, such as a windbox, at a vertical level higher than the first vertical level.

5. A fluidized bed reactor according to claim 2, wherein
15 said second end is at a second vertical level l_2 .

6. A fluidized bed reactor according to claim 4 or 5, wherein the conduit (60, 60', 62, 62') is a mainly upright standpipe, having a bent lower portion connecting said
20 standpipe to the opening (48) in the partition wall (34, 36).

7. A fluidized bed reactor according to claim 1, wherein the conduit is a standpipe having
25 - a lower upward inclined portion, the axis thereof forming a $\geq 30^\circ$ but $< 90^\circ$ angle with the horizontal plane, and
- an upper portion, the axis thereof forming a $> 45^\circ$ angle with the horizontal plane.

30 8. A fluidized bed reactor according to claim 2, wherein
- said second end (50) is connected at a third vertical level l_3 to an opening (52) in an enclosure delimiting said gas source chamber (38'),

35 said conduit having said highest point at an upward bent portion of the conduit, between its first and second end.

9. A fluidized bed reactor according to claim 8, wherein the gas source chamber (38'') is at least partly above the bottom grid (28', 28'') and the first vertical level l_1 is above the third vertical level l_3 .

5

10. A fluidized bed reactor according to claim 1, wherein the solid flow seal is formed by the conduit having

- a first substantially upright conduit portion (46) connected by its lower end to one of said at least one
10 openings (48) at a first vertical level l_1 in a partition wall (34, 36),

- a second substantially upright conduit portion (50) connected by its lower end to an air distributor plate (41) connected to a gas source chamber (38''), such as a
15 windbox, at a third vertical level l_3 , and

- the upper ends of said first and second conduit portions being connected to each other at a second vertical level l_2 , higher than said first level.

20 11. A fluidized bed reactor according to claim 10, wherein the third vertical level l_3 is lower than the first vertical level l_1 .

12. A fluidized bed reactor according to claim 1 or 2,
25 wherein

- the fluidized bed reactor comprises furnace which is divided by a partition into two furnace sections and
- supplying means for introducing gas into the furnace sections are connected to the partition.

30

13. A fluidized bed reactor according to claim 1, wherein

- the fluidized bed reactor comprises two furnace sections separated by a partition, which is a double wall construction, formed of two substantially upright or
35 inclined partition walls delimiting a partition space between them, and

- the supplying means for introducing gas into the furnace

sections are connected to the partition and include

- openings in the partition walls and
- conduits arranged within the partition space and connected by their first ends to said openings in the partition walls and being by their second ends in flow communication with said gas source chamber.

14. A fluidized bed reactor according to claim 13, wherein

- a part of the partition space (39, 39') between the two partition walls forms the gas source chamber, and
- the conduits (60, 60', 62, 62') are standpipes arranged within said gas source chamber.

15. A fluidized bed reactor according to claim 13, wherein

- the partition space is delimited at its vertical sides by the two partition walls (34, 36) and at its bottom by a nozzle supporting plate (41) separating the partition space from the gas source chamber (38''), and
- the conduits (42, 44) arranged within the partition space are connected by their second ends (50) to openings (52) in the nozzle supporting plate (41), for providing gas from the gas source chamber (38'') to the furnace.

16. A fluidized bed reactor according to claim 13, wherein the partition (18) is made of cooling surfaces.

17. A large circulating fluidized bed boiler, comprising a combustion chamber (12) delimited by side walls (22, 24), a bottom grid (28) and a roof, the side walls being made of cooling surfaces, such as finned tube panels or membrane walls, forming a part of the water/steam system of the boiler,

- the combustion chamber being divided by at least one

- division wall (18) reaching mainly from the bottom grid to the roof, for forming two or more separate combustion sections in said combustion chamber, said at least one division wall being made of cooling surfaces connected to
- 5 said water/ steam system of the boiler,
- the lowermost part of the at least one division wall being formed as a dual wall section, the dual wall section being continuous or discontinuous or having solids/ gas flow paths between the separate combustion chamber
 - 10 sections, and
 - a free gas space (38, 39) being formed between the two walls (34, 36) in the dual wall section, and wherein
 - secondary air conduits (42, 44) are provided in the gas
 - 15 space between the walls of the dual wall section, the inlet ends (50) of the conduits being connected to a windbox (38'') and the outlet ends (46) of the conduits to openings (48) in the walls of the dual wall section, for introducing air from the windbox into the combustion sections, and
 - 20 - the secondary air conduits comprising a solid flow seal, preventing solid particles from flowing backward from said combustion section into said conduit in a manner preventing air flow through said secondary conduit.
- 25 18. A fluidized bed boiler according to claim 17, wherein
- the windbox is formed in the free gas space (39', 39'') between the walls of the dual wall,
 - the conduits (60, 60', 62, 62') are disposed in said windbox, and
 - 30 - the conduits are mainly upright standpipes connected
 - by their lower ends (64), which are the outlet ends of the air conduits, at a first vertical level l_1 to openings (48) in the walls of the dual wall section, and
 - 35 - by their upper ends (66) to the windbox, the upper ends being the inlet ends of the air conduits and located at a second vertical level l_2

higher than the first vertical level.

19. A fluidized bed boiler according to claim 18, wherein the height difference Δh between the first l_1 and second l_2 vertical level is about 1.0 m to provide a seal leg by the pressure difference between the windbox and the combustion section.

20. A fluidized bed boiler according to claim 17, wherein

- 10 - the free gas space is divided by a horizontal partition (54) into an upper and a lower free gas space;
- the secondary air conduits (60, 62) in said lower free gas space are connected to a row of openings at a first level in the walls of the partition, and additionally
- 15 - tertiary conduits (60', 62') are provided in said upper free gas space and connected to a row of openings at a second level in the partition.

21. A fluidized bed boiler according to claim 17, wherein

- 20 - the free gas space is divided by a vertical partition.

1/4

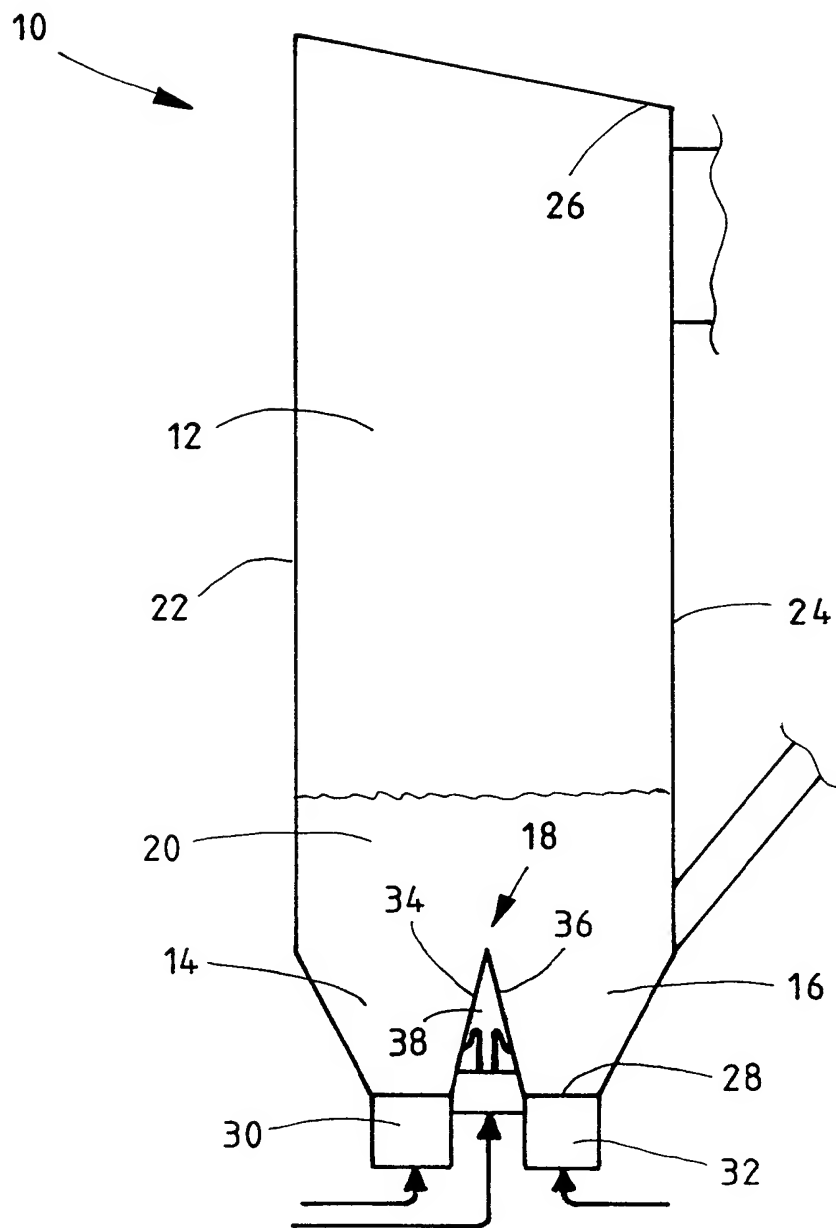


FIG. 1

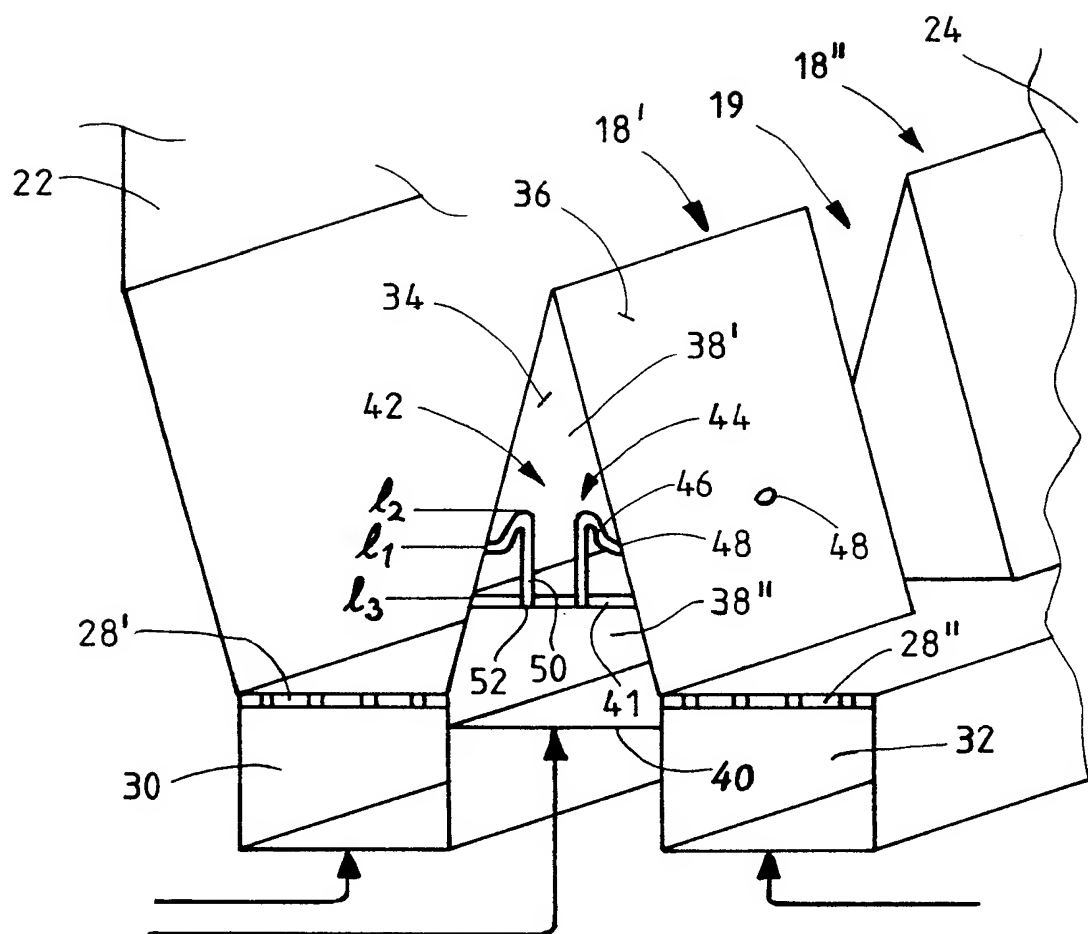


FIG. 2

3/4

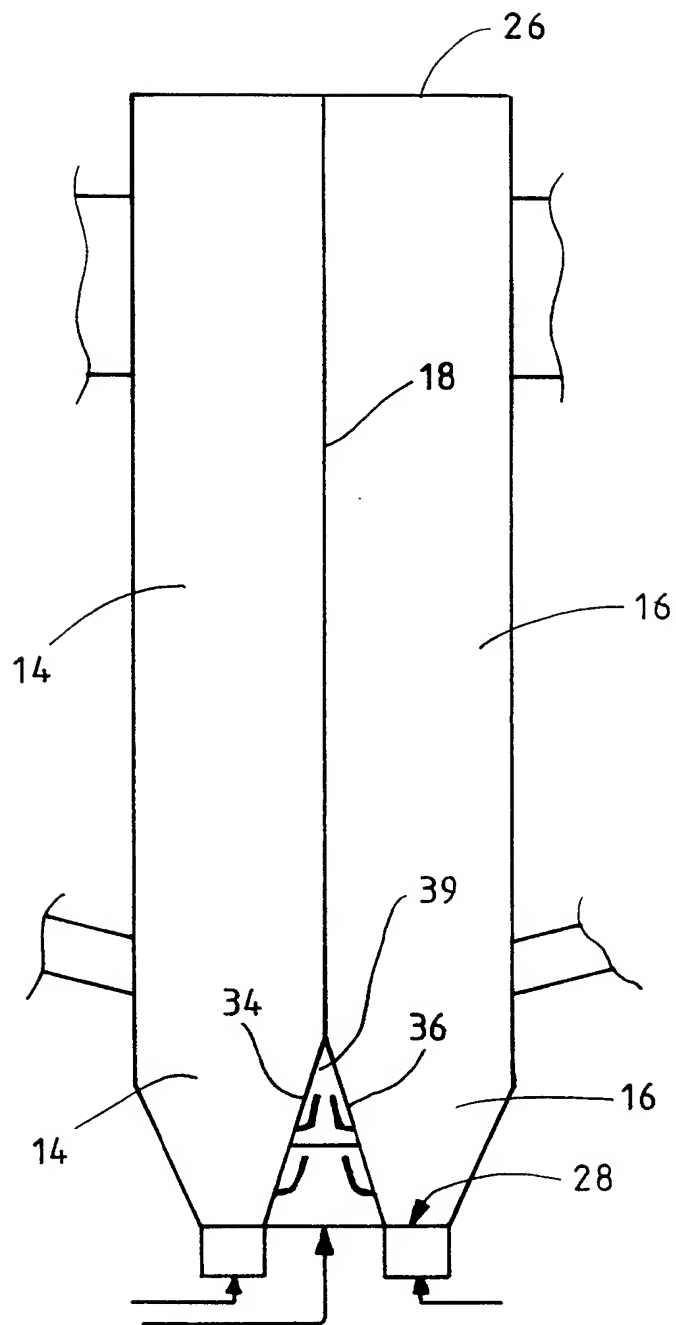
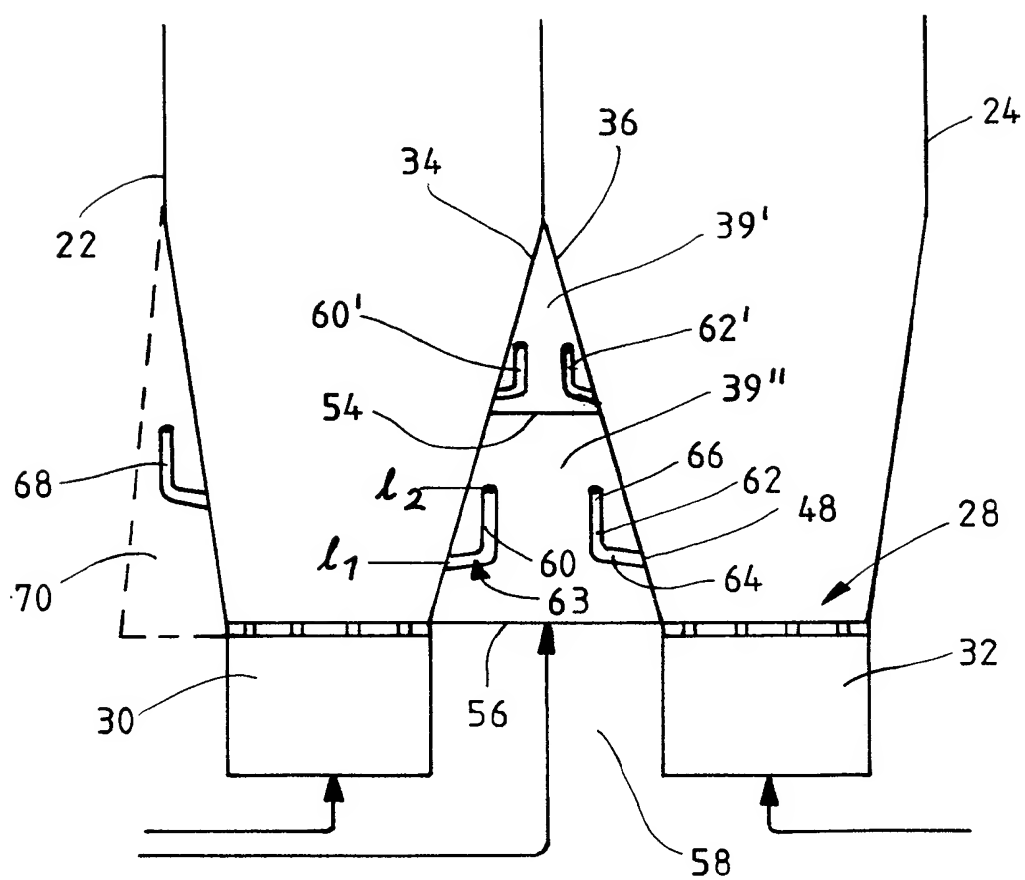
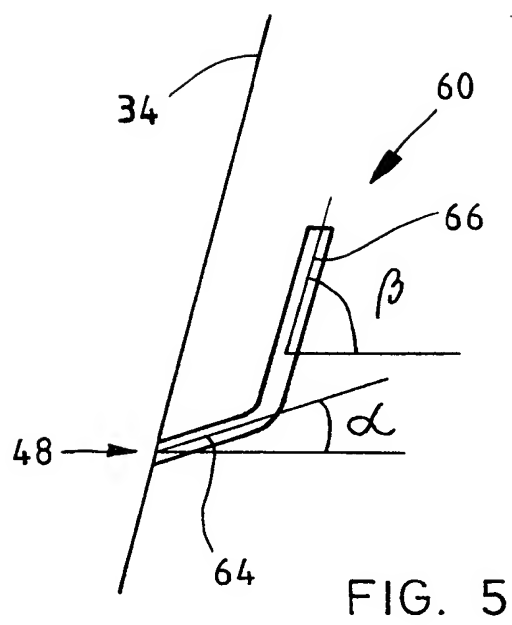


FIG. 3

4/4



INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 98/00560

A. CLASSIFICATION OF SUBJECT MATTER

IPC6: F23C 11/02 // F23L 9/00, B01J 8/24

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: F23C, F23L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	FR 2681668 A1 (STEIN INDUSTRIE), 26 March 1993 (26.03.93), figures 1,2, abstract --	1-7,12,13, 16-19
X	US 4817563 A (BEISSWENGER ET AL), 4 April 1989 (04.04.89), figures 2,3, abstract, details 10,11 --	1-5,12,13,16
X,P	US 5678497 A (GOIDICH), 21 October 1997 (21.10.97), figures 1-5, abstract --	1-3,8,12
X,P	WO 9825074 A2 (THE BABCOCK & WILCOX COMPANY), 11 June 1998 (11.06.98) --	1-5,12-14, 16-18,20

☒ Further documents are listed in the continuation of Box C.☒ See patent family annex.

* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"I" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&" document member of the same patent family

Date of the actual completion of the international search

7 October 1998

Date of mailing of the international search report

13-10-1998

Name and mailing address of the ISA/

Swedish Patent Office

Box 5055, S-102 42 STOCKHOLM

Facsimile No. +46 8 666 02 86

Authorized officer

Anders Bruun

Telephone No. +46 8 782 25 00

INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 98/00560

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0179996 A1 (CORNEL, SCHMIDT GMBH & CO. KG), 7 May 1986 (07.05.86), figure 2, claim 8, abstract --	
A	DE 19501504 C1 (PAULSEN, RALF), 21 March 1996 (21.03.96), figure 2 --	
A	US 4864944 A (ENGSTRÖM ET AL), 12 Sept 1989 (12.09.89), figures 1,2 --	
A	US 4841884 A (ENGSTROM ET AL), 27 June 1989 (27.06.89) -- -----	

INTERNATIONAL SEARCH REPORT

Information on patent family members

27/07/98

International application No.

PCT/FI 98/00560

Patent document cited in search report			Publication date	Patent family member(s)	Publication date
FR	2681668	A1	26/03/93	NONE	
US	4817563	A	04/04/89	AU 589108 B	28/09/89
				AU 1234088 A	01/09/88
				CA 1324881 A	07/12/93
				DE 3706538 A	08/09/88
				DE 3865460 A	21/11/91
				EP 0281165 A,B	07/09/88
				SE 0281165 T3	
				FI 92157 B,C	30/06/94
				FI 880717 A	29/08/88
				IN 165700 A	16/12/89
				JP 2564163 B	18/12/96
				JP 63233204 A	28/09/88
US	5678497	A	21/10/97	NONE	
WO	9825074	A2	11/06/98	NONE	
EP	0179996	A1	07/05/86	DE 3437486 A	17/04/86
DE	19501504	C1	21/03/96	EP 0804705 A	05/11/97
				WO 9622492 A	25/07/96
US	4864944	A	12/09/89	CA 1272870 A	21/08/90
				CN 1010557 B	28/11/90
				EP 0298086 A,B	11/01/89
				SE 0298086 T3	
				FI 84855 B	15/10/91
				FI 861806 A	31/10/87
				IN 169408 A	12/10/91
				JP 1502356 T	17/08/89
				JP 5015923 B	03/03/93
				KR 9605759 B	01/05/96
				LT 2210 A	15/11/93
				LT 73093 R	15/11/93
				SU 1618287 A	30/12/90
				US RE33230 E	12/06/90
				US 4753177 A	28/06/88
				WO 8706678 A	05/11/87

INTERNATIONAL SEARCH REPORT

Information on patent family members

27/07/98

International application No.

PCT/FI 98/00560

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 4841884 A	27/06/89	AU 3682389 A	12/12/89
		DE 68906386 T	11/11/93
		EP 0417153 A,B	20/03/91
		SE 0417153 T3	
		JP 3501580 T	11/04/91
		JP 6042944 B	08/06/94
		WO 8911333 A	30/11/89
<hr/>			